

Headphones

Electroacoustic Design, Verification and Standards

Christopher J. Struck

***CJS Labs
San Francisco, CA – USA***

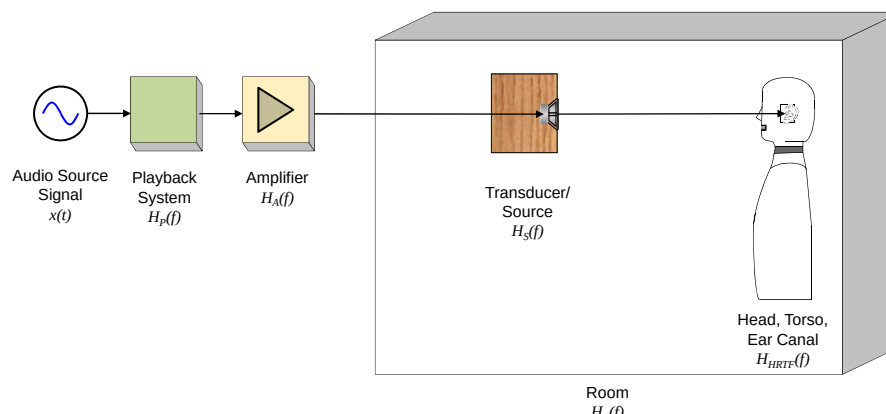
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Overview

- The Insertion Gain Concept
- Orthotelephonic, Free & Diffuse Field Responses
- Acoustic Impedance
- Couplers, Ear Simulators & Manikins
- Electroacoustic Measurements as per IEC 60268-7 & ANSI/ASA S3.7-2016
 - Electrical Impedance
 - Frequency Response
 - Free- and Diffuse Field Corrected Response
 - L-R Tracking
 - Non-Linear Distortion
 - Harmonic, Difference Frequency, Intermodulation
 - Crosstalk
 - Noise Isolation
 - Noise-canceling Headphones
 - Maximum Voltage & Maximum Output

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The Audio Signal Chain

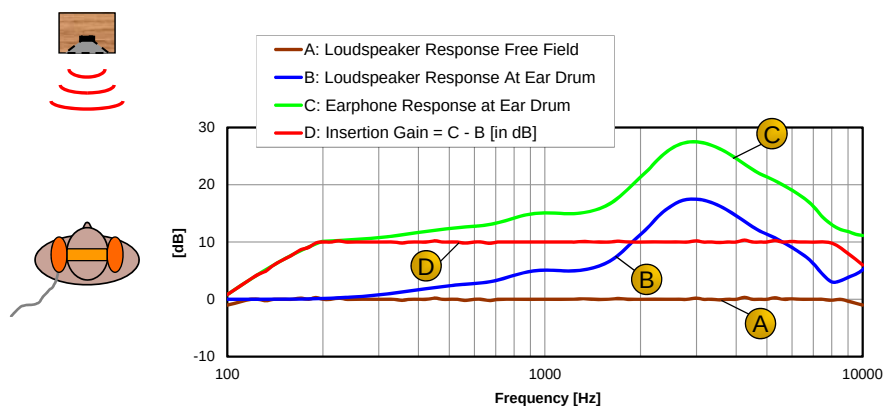


Overall Frequency Response: $H_T(f) = H_A(f) \cdot H_p(f) \cdot H_s(f) \cdot H_R(f) \cdot H_{HRTF}(f)$

Signal at DRP: $x_{DRP}(t) = x(t) \otimes h_p(t) \otimes h_A(t) \otimes h_s(t) \otimes h_R(t) \otimes h_{HRTF}(t)$

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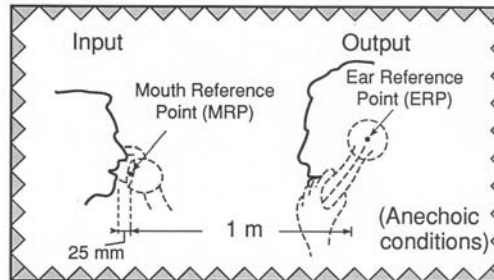
The Insertion Gain Concept



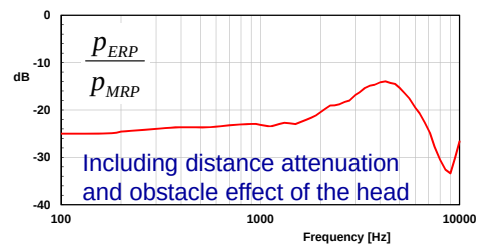
The target is a “flat” Insertion Gain!

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Orthotelephonic Reference

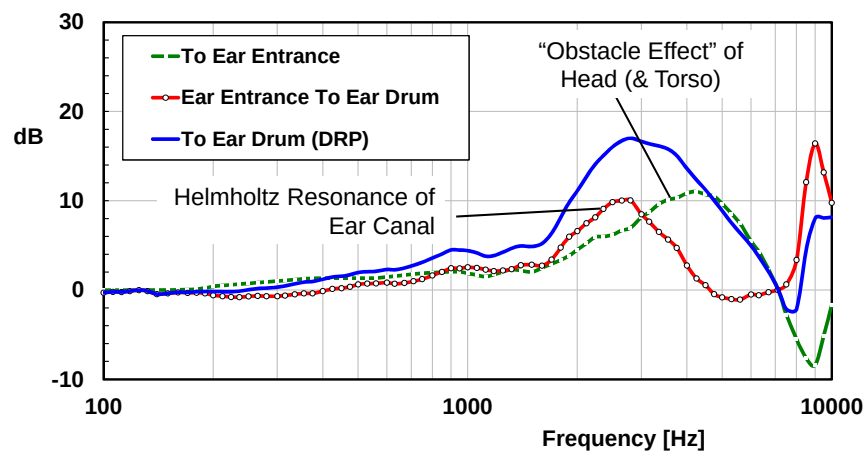


Acoustic transfer function intended to represent a typical conversation



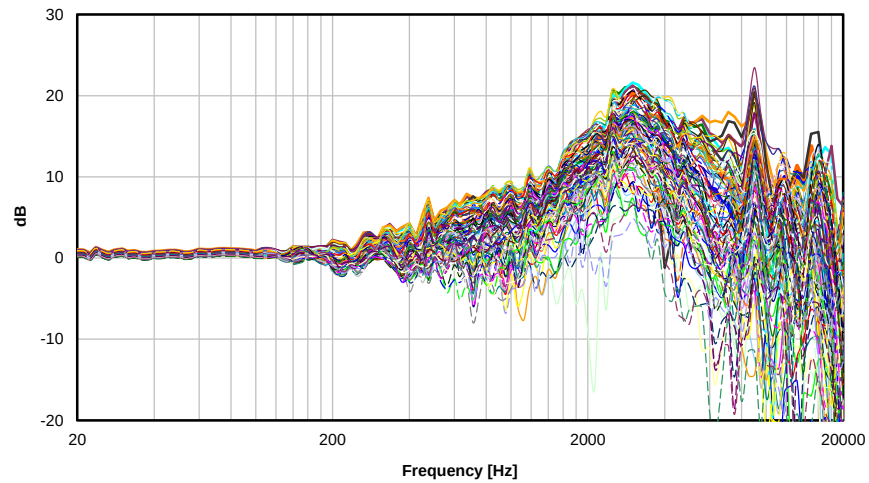
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Components of the Orthotelephonic Response



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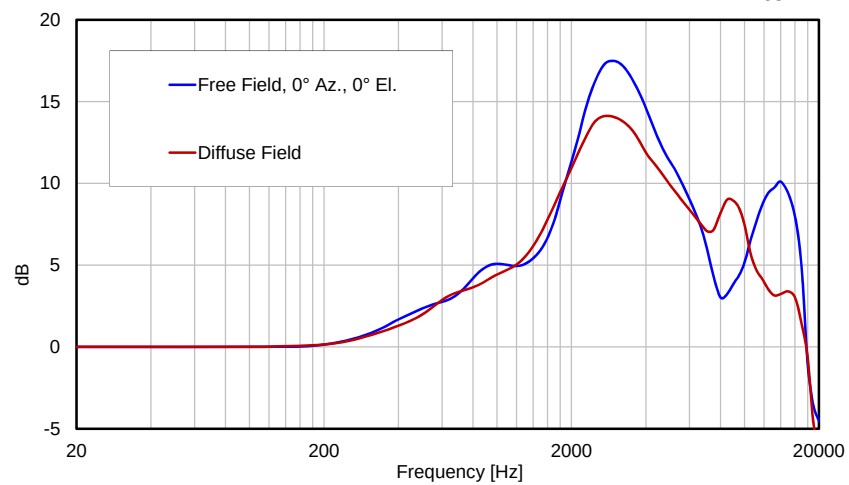
Head Related Transfer Functions



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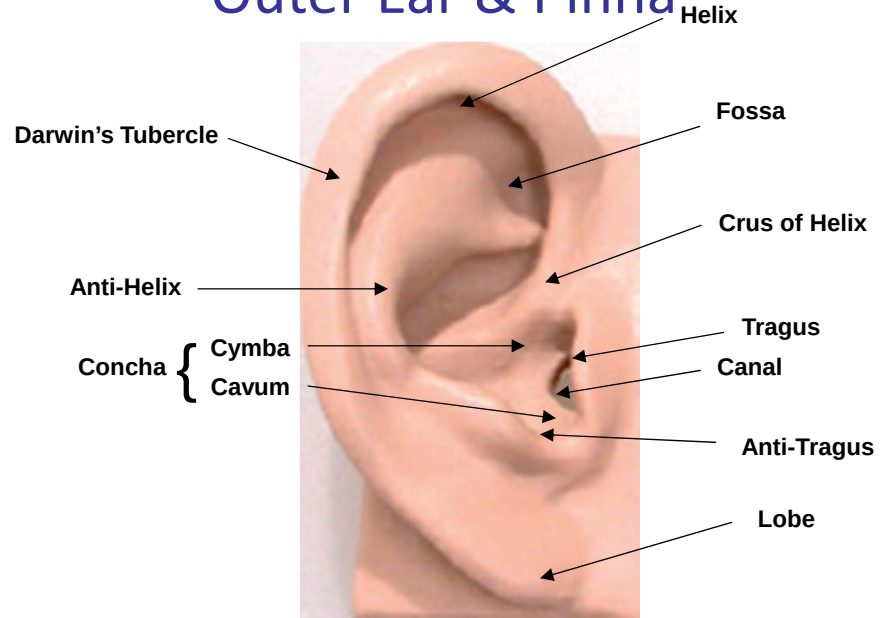
Free & Diffuse Field Responses (at DRP)

IEEE 1652



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Outer Ear & Pinna



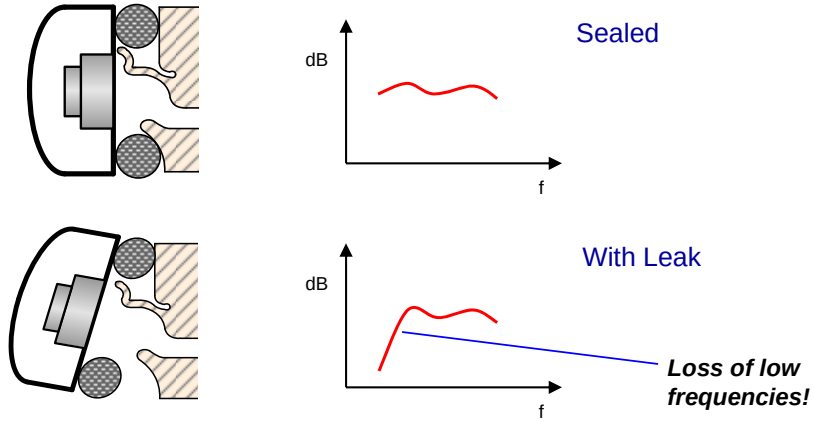
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Earphone Types

Circumaural	Supra-aural	Supra-concha	Intra-concha	Insert

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The Effect of Leakage on Response

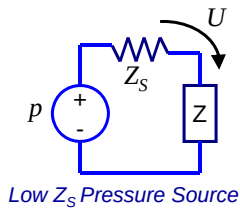


...assuming a high acoustic impedance source

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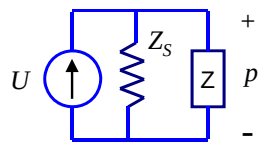
Acoustic Impedance

Thévenin Equivalent



Low Z_s Pressure Source

Norton Equivalent

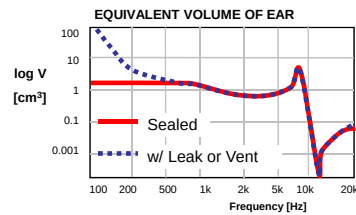
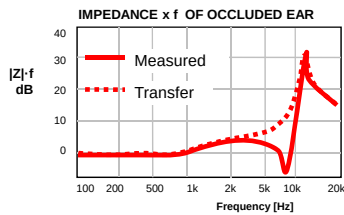


High Z_s Volume Velocity Source

Ohm's Law

$$Z_A = \frac{p}{U}$$

[N·s/m⁵ (mks acoustic ohms)]

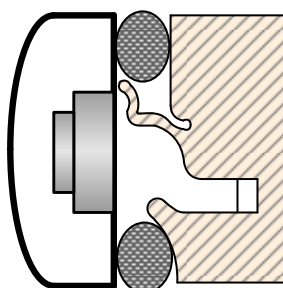


$$\therefore Z_A \cdot f \propto 1 / V_{\text{Equivalent}}$$

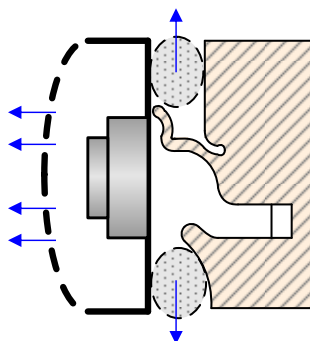
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Acoustical Impedance of Headphones

High Acoustic
Impedance
(Sealed)



Low Acoustic
Impedance
(Open)



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Acoustic Couplers

- Couples measurement microphone to earphone receiver
- Approximates (simplified) acoustic load of ear

A Brief History of some Legacy Couplers:



2cc Coupler
1945 (standardized 1961)
Hearing Aid & Insert Earphone QC/QA

NOTE:
No “reference point”, per se



NBS 9A (6cc)
Coupler
ca. 1950
(standardized ca. 1961)
Audiometer Calibration



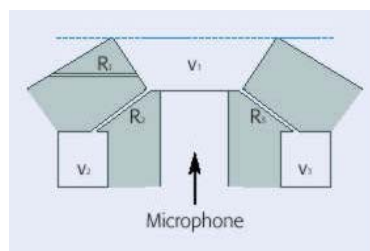
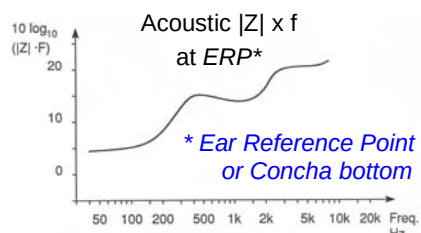
Braun Coupler
ca. 1953
(DIN standard ca.1968)
Telephone Handset
Testing (Legacy)

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Artificial Ear

IEC 60318-1 (ITU-T Type 1)

ca. 1962-68 (standardized 1973)



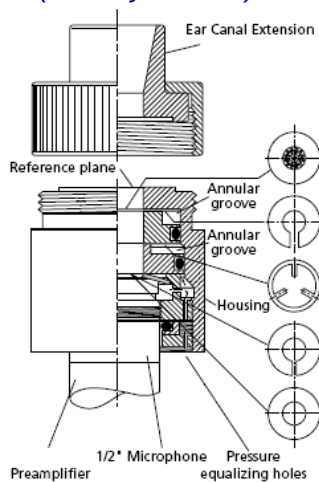
- Audiometer Calibration
- Telephone Handset Testing (Legacy)

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IEC 60318-4 Ear Simulator

(formerly IEC 711)

also ANSI S3.25-2009

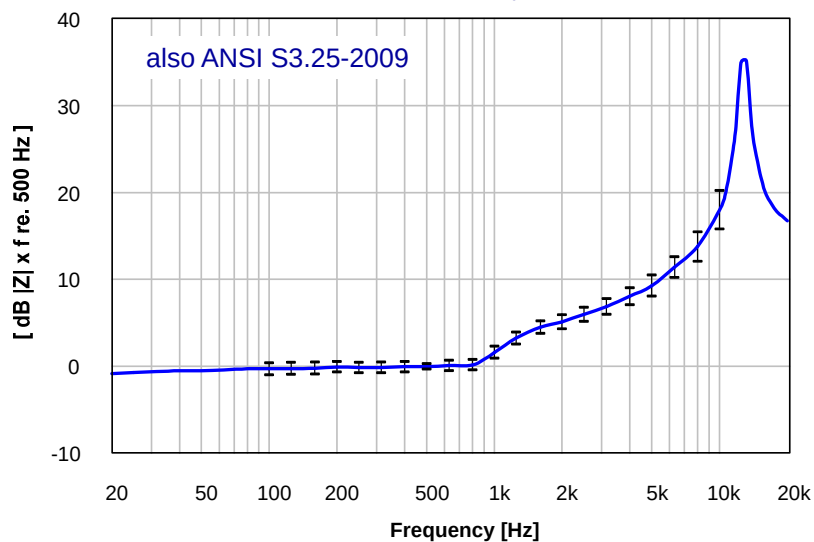


Measurement Microphone Diaphragm is at DRP!

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IEC 60318-4 (formerly 711) Ear Simulator

Acoustic Transfer Impedance



Ear & Cheek Simulator

- Uses IEC 60318-4 (711) Ear
- No Crosstalk or Insertion Response Testing
- Cannot utilize actual headband force
- Retaining force arm may occlude some open-back designs
- Serial Testing of L & R
requires pinna substitution



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QC Test Fixture

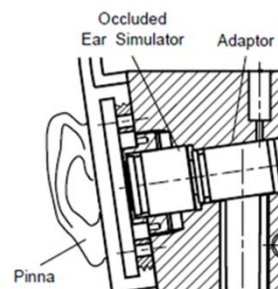


- Can be configured with IEC 60318-4 Ear Simulators
- Crosstalk, Isolation & Insertion Response Test results may differ from manikin tests
- Positioning may be more consistent but less realistic than manikin
- Optimized for QC/QA

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Head And Torso Simulator

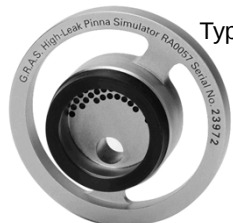
- IEC 60318-4 (formerly 711) Ear Simulators
- Anatomical Pinnæ
- Fulfills IEC 60318-7, ANSI S3.36, and ITU-T Rec. P.58
- Mouth Simulator for headset testing



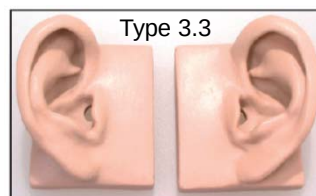
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Pinna Simulators

ITU-T Rec. P. 57 Type 3 (all fitted to IEC 711 Ear)
ca. 1996



Type 3.2



Type 3.3

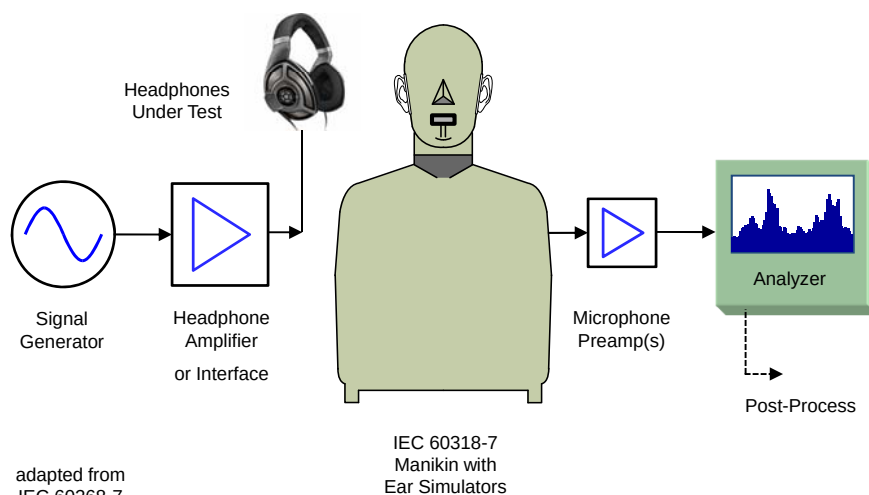


Type 3.4

Type 1 (IEC 60318-1/2) (Legacy)	Sealed High-Z Telephones Audiometer Calibration
Type 2 (IEC 60318-4) Occluded Ear (no pinna)	Insert Earphones
Type 3.2 High Leak / Low Leak	Hard Earcap Telephones
Type 3.3 Soft Anatomical (HATS)	All Types. Most Realistic.
Type 3.4 Simplified Soft Anatomical	Handset Telephones Binaural Recording

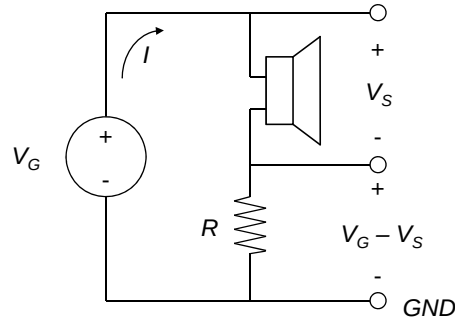
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Basic Test System



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Electrical Impedance



For $R \ll 0.1 |Z_{MIN}(f)|$ (typically 0.1Ω):

$$Z(f) = \frac{V_S(f) R}{V_G(f) - V_S(f)}$$

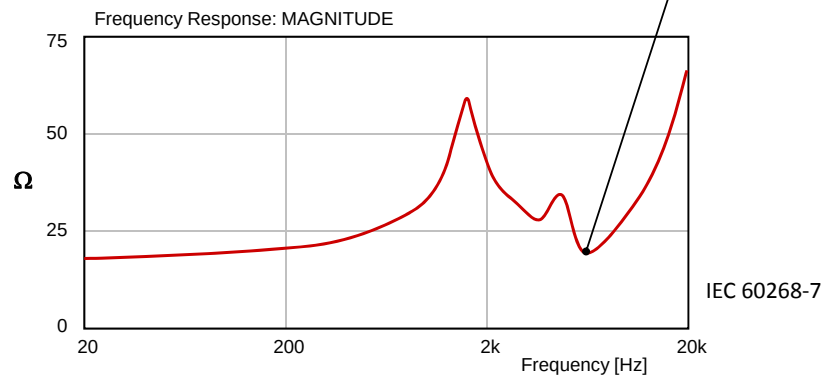
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Electrical Impedance

- Low Voltage (LINEAR!)
- R40 40th decade (1/12 octave) stepped sine
- Can also measure phase, if desired
- Measured with headphones on manikin!
- For 'standard' impedances (e.g., 16, 32, etc.), R_{DC} is often a good indicator of Z_{MIN} & Z_0 !

$$Z_{MIN} \geq 0.8 Z_0 !$$

$$Z_0 \geq 1.25 Z_{MIN}$$



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Source Output Impedance

- IEC 60268-7 Specification:
 $Z_{OUT} = 120 \Omega$
- Actual headphone amplifiers vary from
 $< 1 \Omega$ to $> 100 \Omega$
- ∴ Recommend measuring at both 120Ω AND 1Ω

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Test Conditions

- **Characteristic Voltage:** The sinusoidal voltage at 500 Hz (or IEC 60268-1 simulated program signal*), applied through the rated source impedance (120 ohms), to obtain a sound pressure level of 94 dB SPL in the ear simulator (with or without A-Weighting).
 - **NOTE: Some devices for portable music players may not be capable of producing 94 dB SPL!**
- **Rated Source Voltage:** Maximum specified RMS voltage which should be applied to the headphone through the rated source impedance, during the reproduction of normal program signals. NOTE: For headphones complying with IEC 61938, Rated Source Voltage = 5 V. Preferably, should not exceed the Characteristic Voltage by more than 15 dB.

* Only applicable to systems with integral signal processing for IEC 60268-7. Required for EN 50332.

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Test Conditions

- **Working Sound Pressure Level:** SPL resulting from a sinusoidal voltage (single figure at 500 Hz or simulated program signal) through the rated source impedance (120 ohms), across the input connector of the headphone, *at a level such that would cause 1 mW to be dissipated in a pure resistance equal to the rated impedance of the headphone.*

Voltages for 1 mW for Nominal Impedance, Z_0 :

16 Ω : 126 mV	60 Ω : 245 mV	250 Ω : 500 mV
20 Ω : 141 mV	80 Ω : 283 mV	300 Ω : 548 mV
25 Ω : 158 mV	100 Ω : 316 mV	400 Ω : 632 mV
32 Ω : 179 mV	120 Ω : 346 mV	500 Ω : 707 mV
40 Ω : 200 mV	160 Ω : 400 mV	600 Ω : 775 mV
50 Ω : 224 mV	200 Ω : 447 mV	

- **Maximum Sound Pressure Level:** SPL produced in the ear simulator when the headphone is supplied with a sinusoidal voltage of the Rated Maximum Voltage at 500 Hz (see also EN 50332).

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Ohm's Law

$$V = IR, P = VI$$

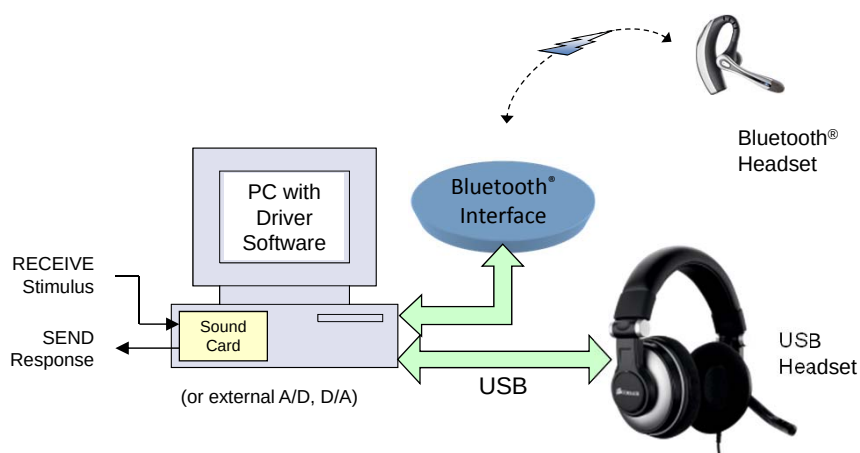
$$P = \frac{V^2}{R} = \frac{V^2}{Z_0}$$

$$V^2 = PZ_0$$

$$V = \sqrt{PZ_0} = \sqrt{0.001 \cdot Z_0}$$

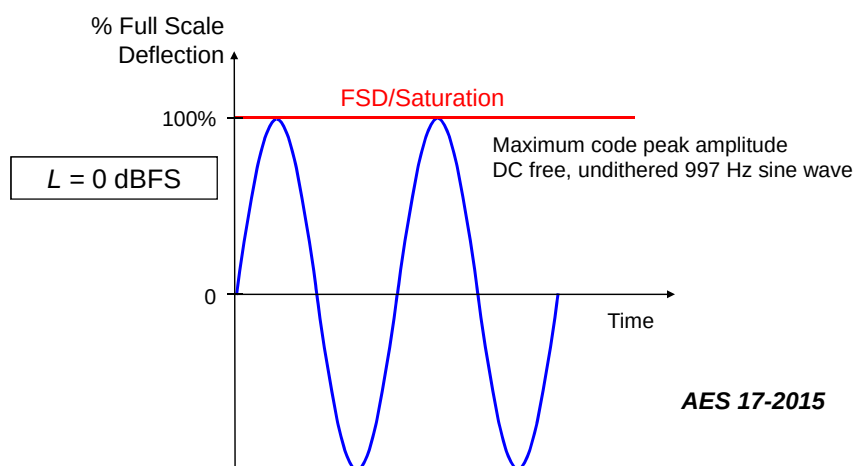
$$V = 0.0316 \sqrt{Z_0}$$

Interfacing to a Bluetooth® or USB Device



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Digital Levels: 0 dBFS



NOTE 1: This is +3.01 dB re. the RMS level for a unity peak amplitude sine wave and is equivalent to a dB reference of 0.707.

NOTE 2: $L = +3.01$ dBFS for a square wave of the same peak amplitude.

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- What is it?
 - A low power, low data rate digital wireless communication protocol
 - Device types include computer mice, keyboards, medical monitors, loudspeakers, headphones, headsets, etc.
 - Each device classification has its own “profile”
 - Communication is asynchronous – There is no master clock
 - May require additional processing (sample rate conversion, frequency alignment) before analysis
- Relevant Audio Profiles:
 - **A2DP**: Unidirectional Music Playback, 16-48 kHz Stereo
 - **HPF/HSP**: Bidirectional Voice Communication, 8-16 kHz Mono
- More info at: <https://www.bluetooth.com/>

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Bluetooth® Pairing

1. Inquiry
 - Bluetooth® Device broadcasts an ID beacon, then waits for other devices to respond.
2. Discovery & Authentication
 - After discovery, devices exchange features they support and authenticate, generally by Simple Secure Pairing Protocol
3. Exchange of Link Keys
 - The link keys are encrypted tokens that ensure the Bluetooth® connection remains private

Pair By Name

After Inquiry, pair with the first device that matches the specified name

Pair By Address

Skips Discovery and proceeds immediately with Link Key exchange

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Non-Concurrent Stimulus-Capture-Analysis

For Devices with:

- Input and Output in different domains
 - E.g., Digital Input, Analogue Output
- Access to only Output (Playback) **OR** only Input (Recording)
- Different sample rates or asynchronous Input & Output
- Unstable delay and/or phase between Input and Output

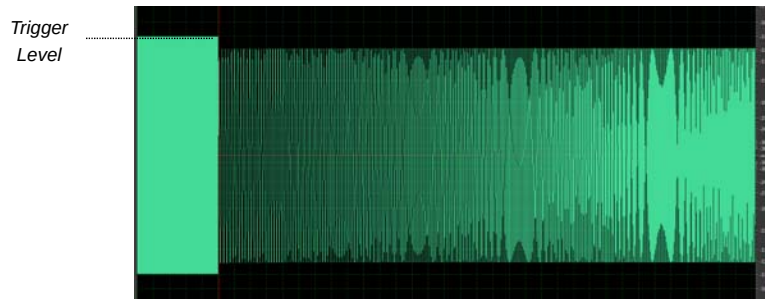
The following additional steps may be required:

- Pre-Conditioning Tone & Triggered Analysis
- Sample Rate conversion
- Frequency re-alignment
- Time window or edit/trimming of captured waveform

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Pre-Conditioning Tone

- Typically a short burst of a mid-band tone preceding the actual test stimulus, e.g., 1 kHz for 250 ms
- Used to:
 - Bias the DUT into a quasi stable state
 - Synch/align the DUT clock and sample rate to the analysis sample rate
 - Trigger the *start* of a data capture (but ignored in the analysis)

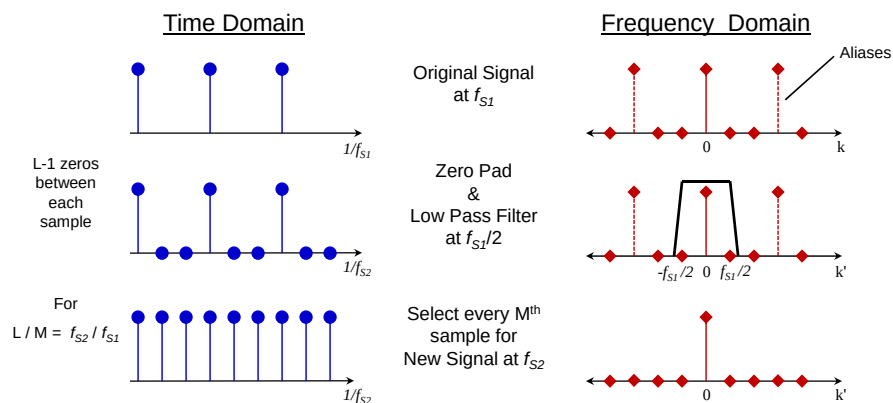


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Sample Rate Conversion

- Required for asynchronous I/O systems, even if the stated sample rate matches the analysis!

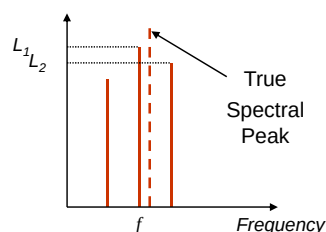
Conversion between two sample rates $f_{S1} < f_{S2}$:



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Frequency Alignment

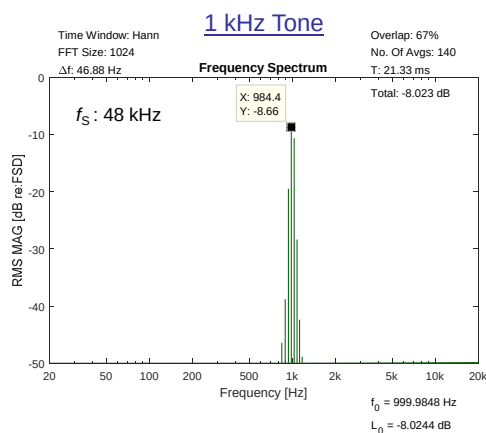
- Scale frequency response to the true frequency of the conditioning tone
- Requires frequency resolution beyond Δf of the FFT



For pure tones & Hann Weighting:

$$f_{\text{TRUE}} = f + f_C$$

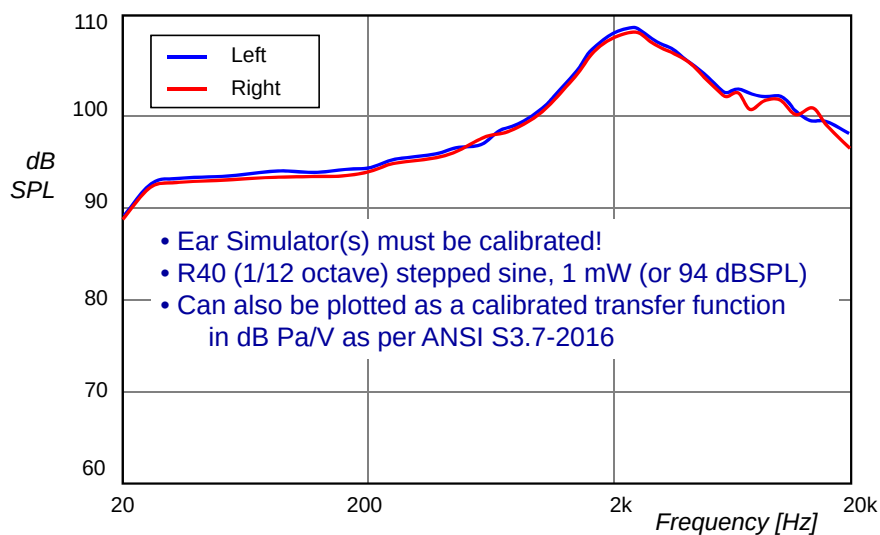
$$\text{where } f_C = \frac{2 - 10^{(L_1 - L_2)/20}}{1 + 10^{(L_1 - L_2)/20}} \cdot \Delta f$$



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Frequency Response

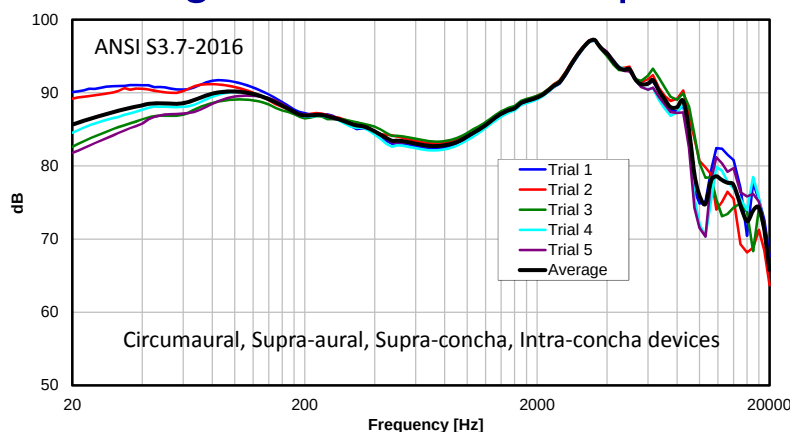
1 mW Input



- Ear Simulator(s) must be calibrated!
- R40 (1/12 octave) stepped sine, 1 mW (or 94 dB SPL)
- Can also be plotted as a calibrated transfer function in dB Pa/V as per ANSI S3.7-2016

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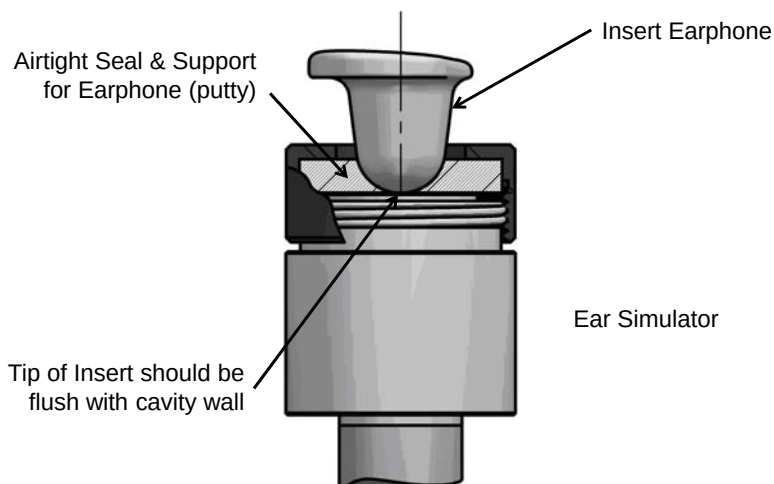
Positioning Errors & Test Repeatability



- Test/Re-Test: dB Average of 5 re-positions:
 - Complete removal and re-installation!
 - Reject re-positions $> \pm 2$ dB (500Hz – 5 kHz)
 - Check low frequency response for leakage
 - Report Average & Max σ

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Coupling Sealed Insert Earphones

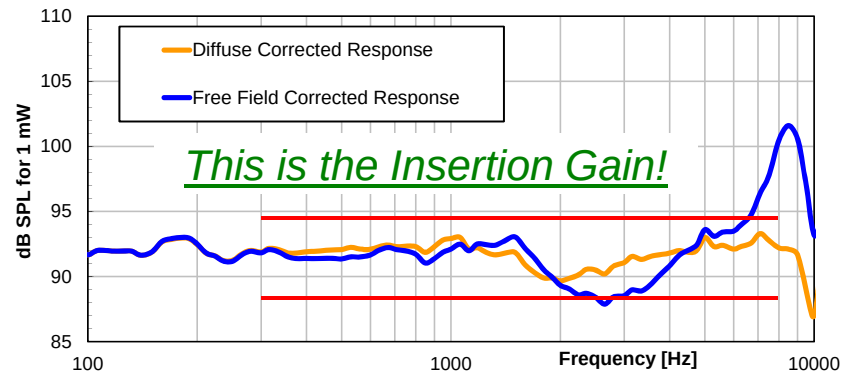


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Diffuse & Free Field Corrected Response

$$\text{DIFFUSE: } H_{DFC}(f) = H(f) - H_{\text{Diffuse}}(f) \quad [\text{in dB}]$$

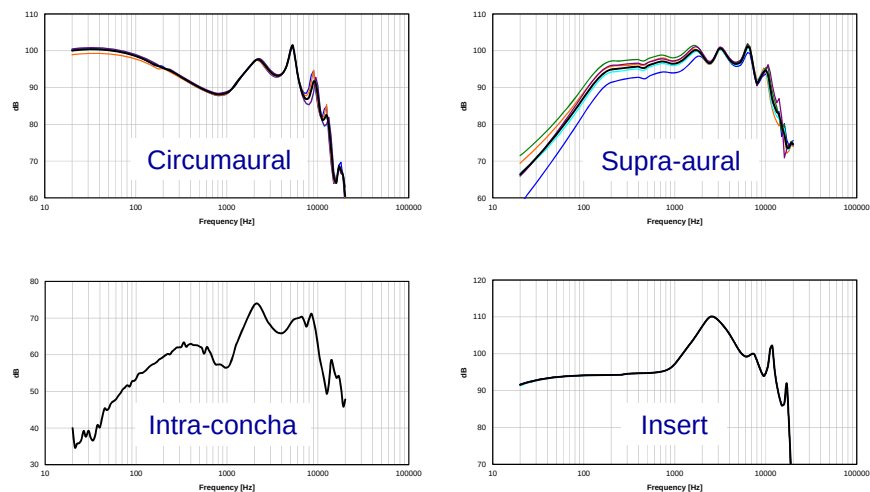
$$\text{FREE FIELD: } H_{FFC}(f) = H(f) - H_{FF\ 0^\circ, 0^\circ}(f) \quad [\text{in dB}]$$



- Maps to perceived response
- Simplifies visualization and tolerance application
- Important range: 300 Hz – 8 kHz

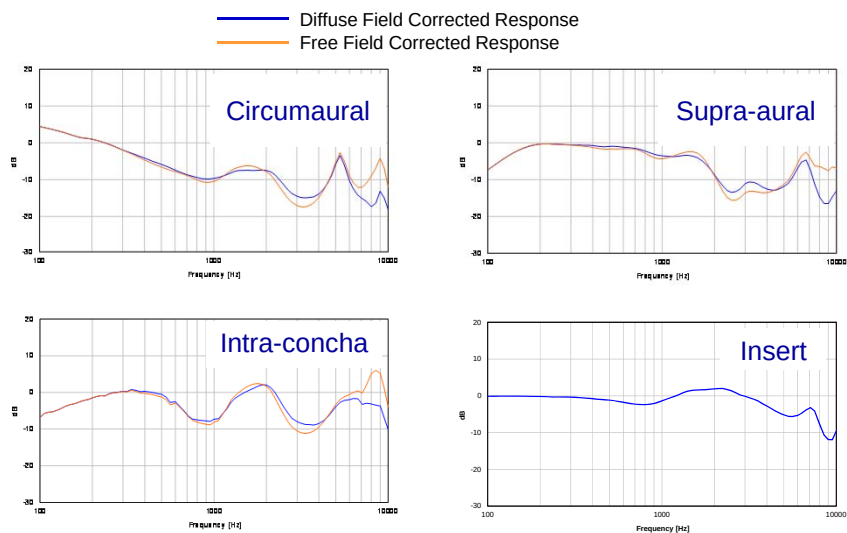
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Measured Responses at DRP



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Resulting Insertion Gain



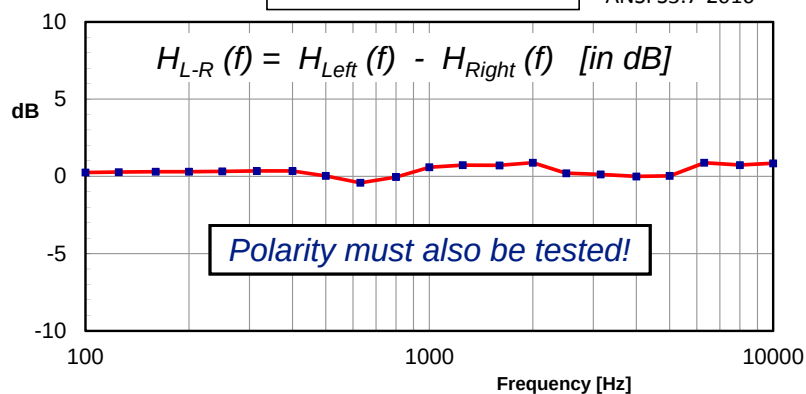
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Left-Right Tracking

L & R Responses are 1/3 octave power averaged in each band:

$$L(f) = 10 \log_{10} \frac{1}{N} \sum_{i=1}^N 10^{L_i/10}$$

ANSI S3.7-2016



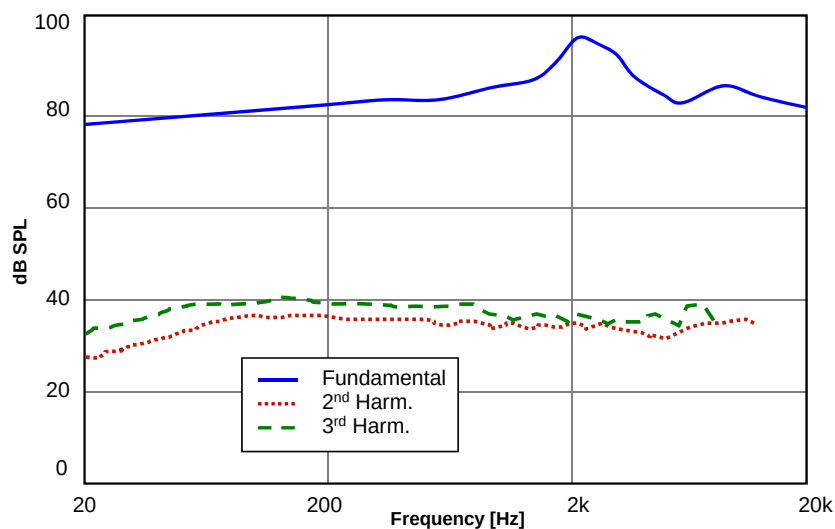
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Polarity Test Methods

- Low Frequency Phase comparison
 - $\phi(f)$ asymptotes toward 0° or 180°
- $H_L(f) + H_R(f)$ complex summation
 - Magnitude: +6 dB or noise floor
 - Change in shape of Lissajous figure
- Time Domain Pulse
 - Positive or negative going waveform

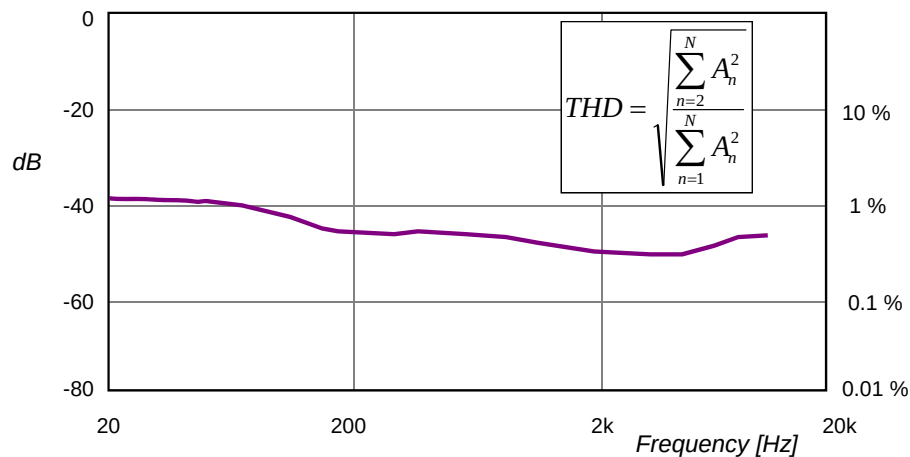
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Harmonic Distortion at Rated Voltage



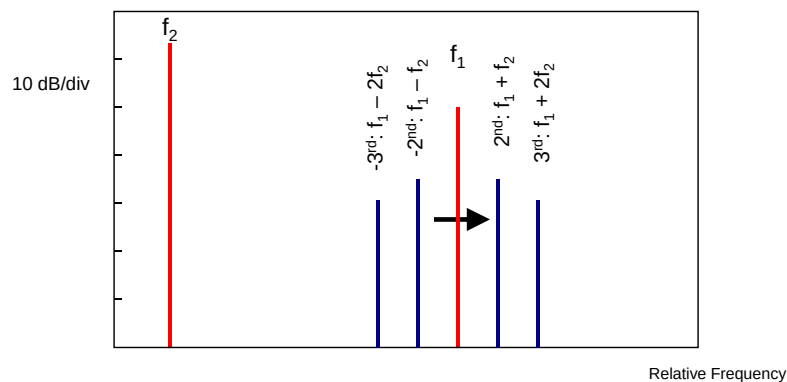
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THD vs. Frequency



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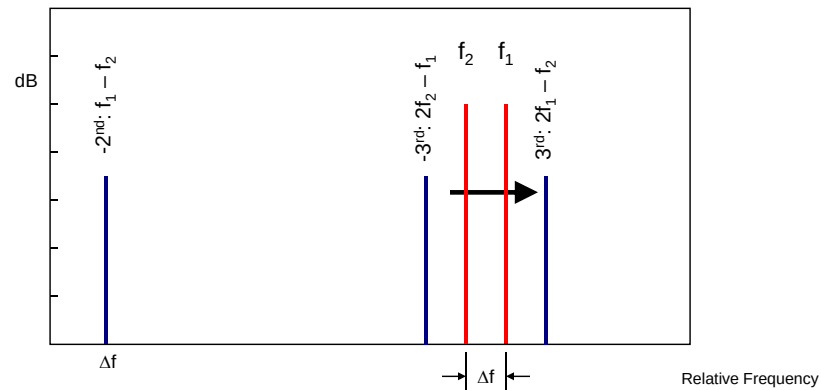
Intermodulation Distortion



- f_2 low frequency fixed tone at -1.9 dB re: Rated Voltage at 70 Hz
- f_1 tone at -14 dB (4:1) at 600 Hz OR stepped or swept
- f_2 is the frequency interval between distortion products
- IM products follow f_1 as a group

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Difference Frequency Distortion



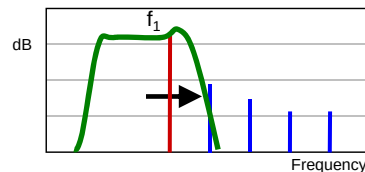
- f_1 & f_2 each at -6 dB re: Rated Voltage, stepped or swept.
- $\Delta f = f_1 - f_2 = 80$ Hz
- Δf is the frequency interval between distortion products
- Odd-order products follow as a group with f_1 & f_2 . Even order products fixed.

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Distortion Measurements in Band Limited Systems

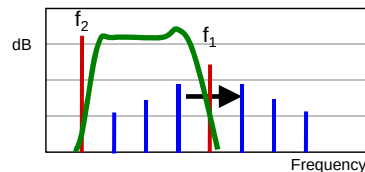
Harmonic Distortion

- Most Harmonics above passband
- Does not excite higher order non-linearities



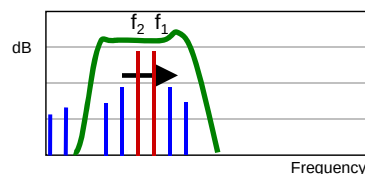
Intermodulation Dist.

- f_2 below passband OR IM products outside passband



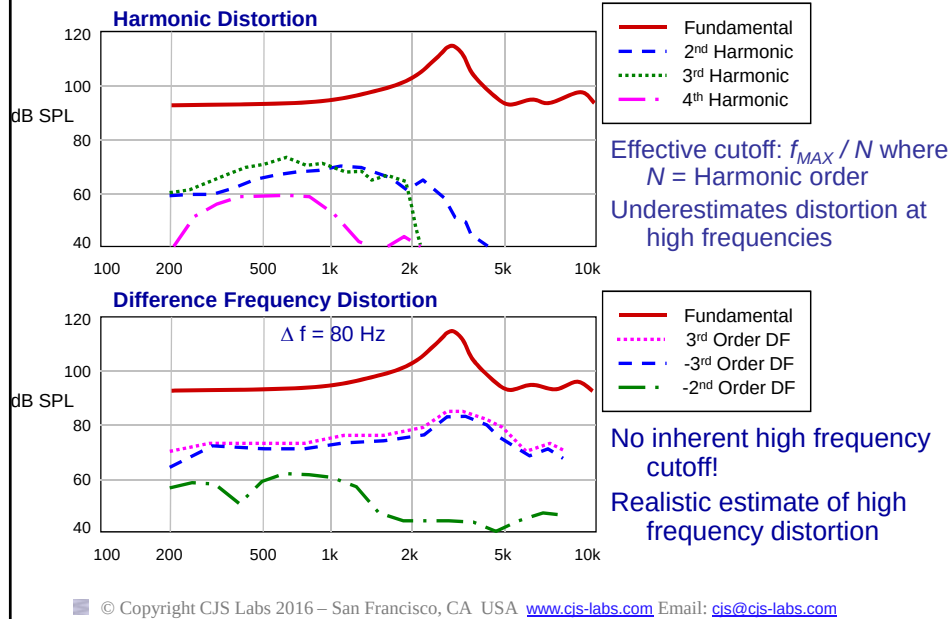
Difference Frequency Dist.

- Odd-order products within passband
- Even-order products may be inside or outside passband

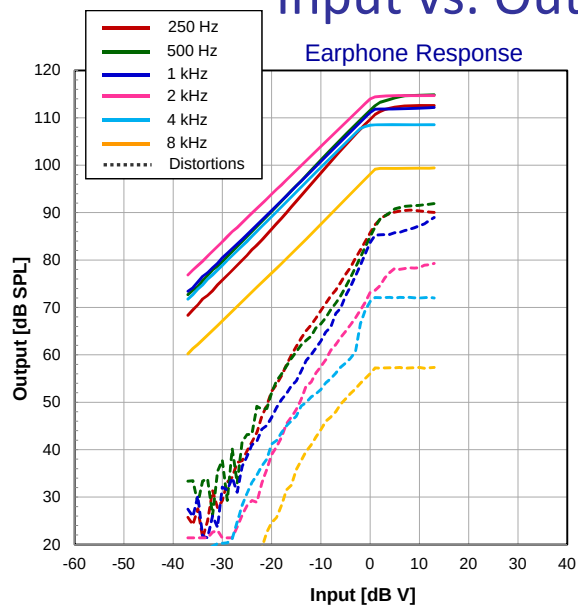


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Diff. Freq. vs. Harmonic Distortion



Input vs. Output



- Traditional measure of linearity
- Step size: 1 dB
- Tested at multiple frequencies, but limited frequency information
- Linear is at 45° for correct aspect ratio
- Upper "knee" point shows linearity limit
- Total Distortion is the power sum of the 2nd & 3rd Harmonics

ANSI S3.7-2016

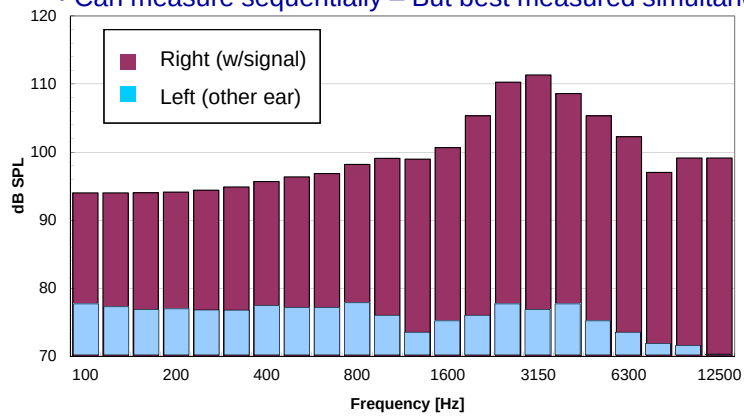
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Crosstalk

- Requires 2 Ear Simulators
- Measurement S/N is poor:
 - Use 94 dB SPL sinusoidal test signal
 - Convert to 1/3 octave as power summation*
 - Check background noise level (≤ -10 dB in each band!)
- Can measure sequentially – But best measured simultaneously

In each 1/3 octave band:

$$L(f) = 10 \log_{10} \sum_{i=1}^N 10^{L_i/10}$$



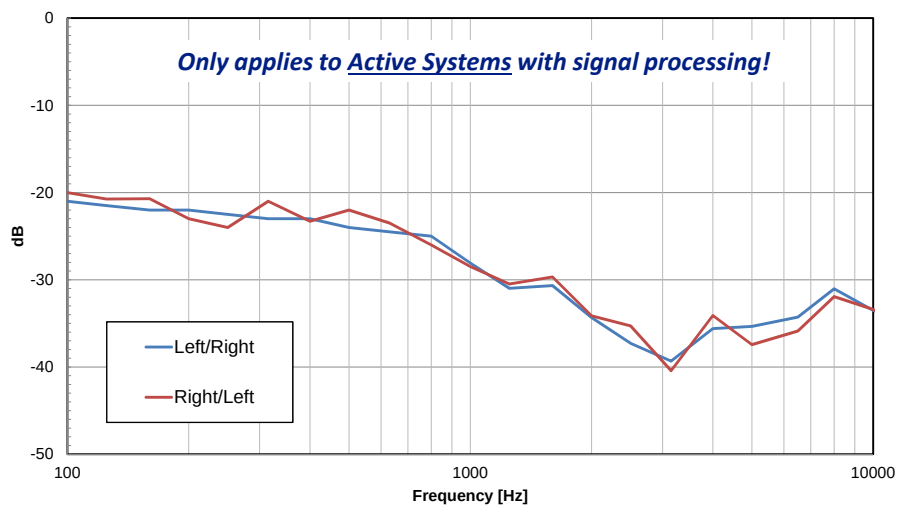
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Crosstalk

$$C_{L-R}(f) = G_{L/R}(f) - G_{R/R}(f) \text{ [in dB]} \text{ for signal applied to RIGHT Ear}$$

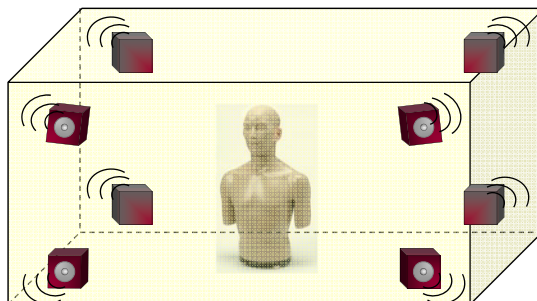
$$C_{R-L}(f) = G_{L/R}(f) - G_{R/R}(f) \text{ [in dB]} \text{ for signal applied to LEFT Ear}$$

Only applies to Active Systems with signal processing!



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Noise Isolation

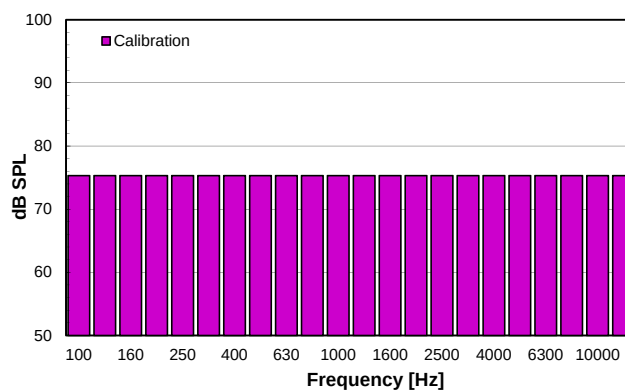


Diffuse Noise Field

- Reverberant Room and/or Uncorrelated Sources
- 90 dB SPL at Test Point

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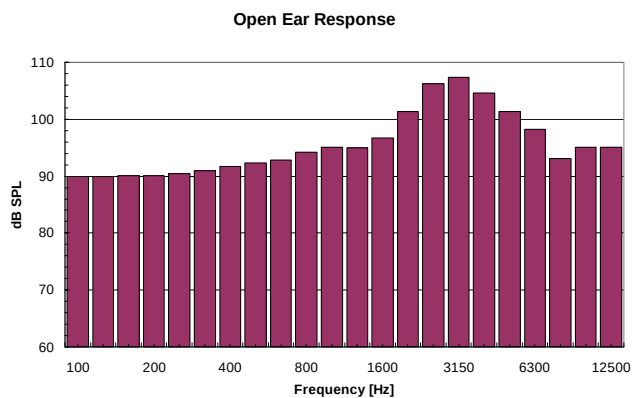
Noise Isolation - 1



90 dB SPL Pink Noise w/ Real-time Filter Analysis OR FFT + 1/3 Octave Synthesis

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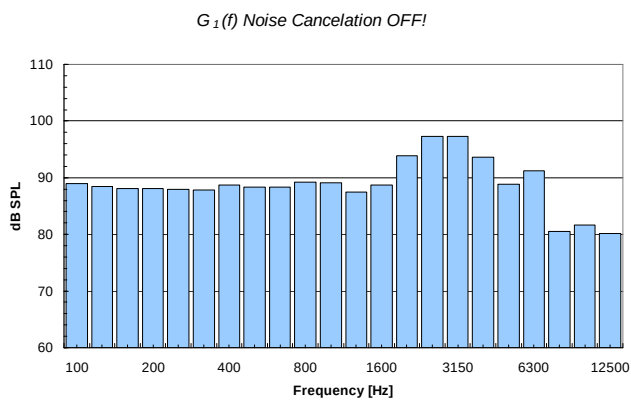
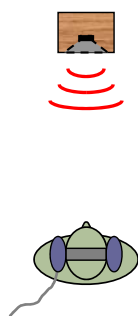
Noise Isolation - 2



90 dB SPL Pink Noise w/ Real-time Filter Analysis OR FFT + 1/3 Octave Synthesis

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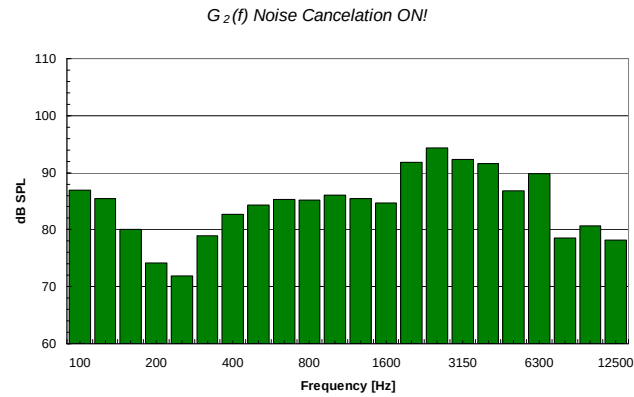
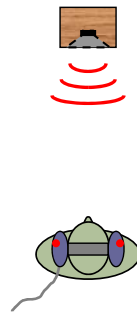
Noise Isolation - 3



90 dB SPL Pink Noise w/ Real-time Filter Analysis OR FFT + 1/3 Octave Synthesis

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Noise Isolation - 4



90 dB SPL Pink Noise w/ Real-time Filter Analysis OR FFT + 1/3 Octave Synthesis

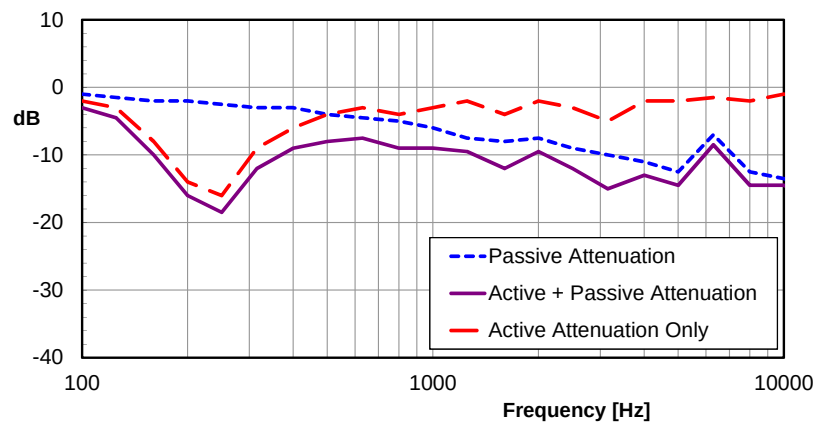
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Noise Isolation

$$L_{\text{Passive}}(f) = G_{\text{NR-OFF}}(f) - G_{\text{Open Ear}}(f) \quad [\text{in dB}]$$

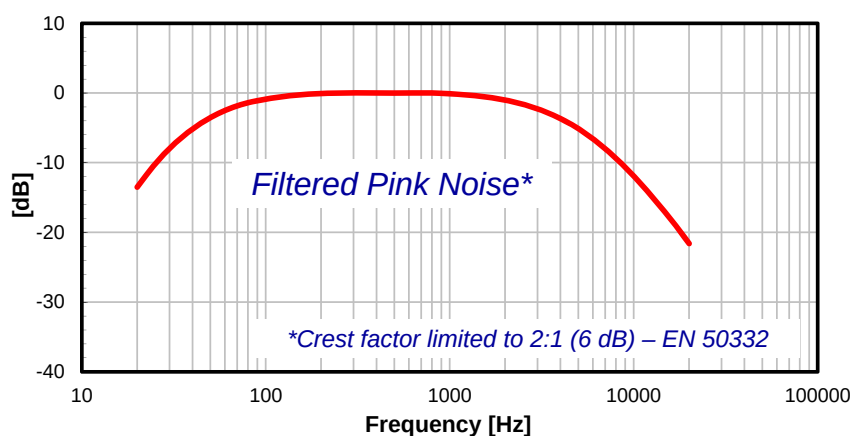
$$L_{\text{Active + Passive}}(f) = G_{\text{NR-ON}}(f) - G_{\text{Open Ear}}(f) \quad [\text{in dB}]$$

$$L_{\text{Active}}(f) = L_{\text{Active + Passive}}(f) - L_{\text{Passive}}(f) \quad [\text{in dB}]$$



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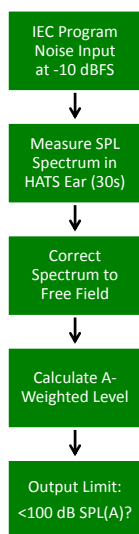
IEC 60268-1 Simulated Program Spectrum



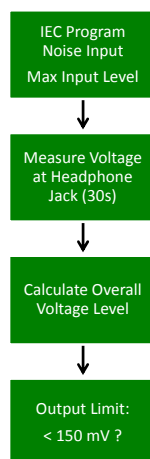
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EN 50332 Maximum Output

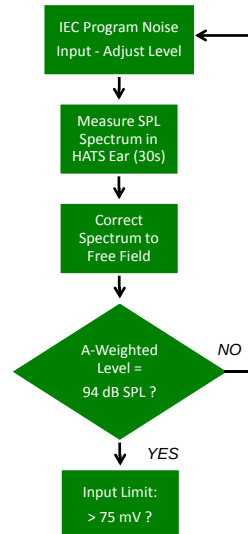
EN 50332-1: System



EN 50332-2: Player



EN 50332-2: Earphones



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Maximum Voltage

- Maximum RMS voltage of the IEC 60268-1 program noise signal, limited to a crest factor between 1.8 and 2.2, through the rated source impedance, which the headphone can tolerate without *permanent damage**
- **Rated Long-Term Maximum Voltage:**
 - Signal applied for 10 periods of 60s *ON*, 120s *OFF*
 - *No change in specs after 4 hours of rest/storage
- **Rated Maximum Permanent Noise Source Voltage:**
 - Signal applied continuously for 100 hours!
 - *No change in specs after 24 hours of rest/storage

NOTE: THIS IS A DESTRUCTIVE TEST!

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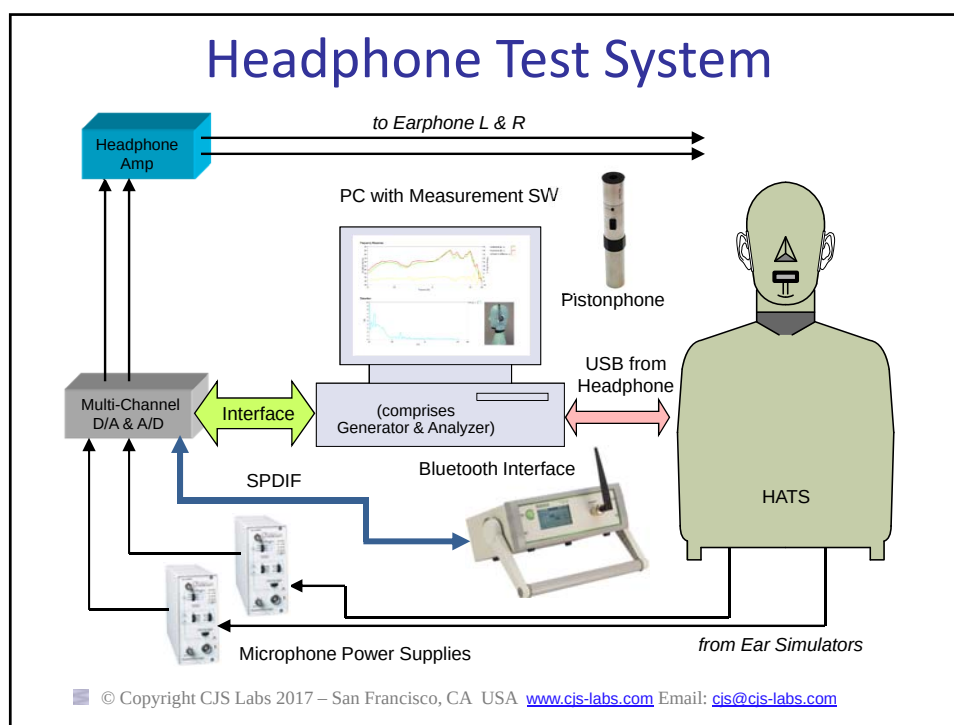
A Minimum Test Suite

- L & R Frequency Response¹
 - Show Mean and all re-position trials
- Left-Right Tracking
- Free and Diffuse Field corrected responses
- L & R Harmonic Distortion²

¹Test level, and nominal electrical impedance (if applicable) should also be reported

²Assumes 2-tone distortion test capability is not available.

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Conclusion (1)

- Insertion Gain
 - A *FLAT INSERTION GAIN* is the target!
 - This is 'corrected' from the measured response at *DRP*.
- Acoustic Impedance
 - Low Acoustic Z = Open
 - High Acoustic Z = Sealed
- Test System and Tests
 - Requires a manikin equipped with calibrated ear simulator(s)
 - Sine *AND* Noise stimuli may be required
 - FFT Data requires 1/3 octave synthesis (power averaging)
 - Most post-processing is simple dB subtraction
 - Present data using the IEC 60263 preferred aspect ratio:
 - 10, 25, or 50 dB = 1 decade

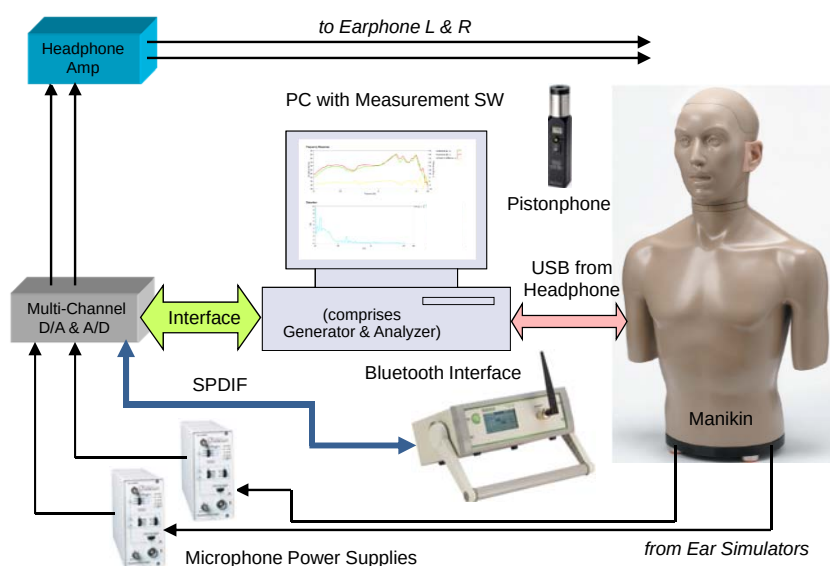
Conclusion (2)

Vis-à-vis IEC 60268-7 {Ed. 3.0} 2010-1:

- 120Ω amplifier Z_{OUT} not representative in many cases
- Average of 5 trials can mitigate positioning errors
- Free & Diffuse Field responses provide useful estimates (bounds) of perceived response, i.e., the insertion gain
- Left-Right Tracking in 1/3 octaves correlates to loudness match. Polarity is also important!
- I/O response reveals range of linearity vs. input level
- 2-Tone distortion tests are a realistic indicator of non-linearity in band-limited systems
- ANSI/ASA S3.7-2016 incorporates most of these refinements

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Headphone Test System



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